EM 3 Section 17: Summary of EM in media; boundary conditions on fields

17. 1. Effect of Magnetic Materials on Inductance

First we have to finish off our description of magnetism with a look at how inductance is affected by magnetisation currents

Example: conducting core in solenoid "A long solenoid of *n* turns per unit length, length ℓ and cross sectional area \mathcal{A} is filled with ferrite, in which \underline{M} obeys $\underline{M} = \chi_m \underline{H}$ where $\chi_m = 900$. Find the self inductance L."

Recall the definition $L = \Phi_B/I$ this stems from Faraday's law MIII, and is therefore **un**changed by media. Ampère's law in the static situation $\partial \underline{D}/\partial t = 0$ becomes

in integral form where I is the usual conduction current. Now note the symmetry: \underline{H} is axial within the solenoid and vanishes outside for large ℓ . Taking a loop as shown in figure,

Figure 1: Solenoid with conducting core: Amperian loop

H = nI, so <u>M</u> is axial; magnitude $M = \chi_m nI$ Then B also must be axial:

$$B = \mu_0(H + M) = (\chi_m + 1)\mu_0 nI$$

$$\Rightarrow \Phi_B = n\mathcal{A}LB = (\chi_m + 1)\mu_0 n^2 \mathcal{A}LI$$

$$\Rightarrow L = \Phi_B/I = (\chi_m + 1)\mu_0 n^2 \mathcal{A}\ell$$

Thus L is 901 times larger than in vacuum (vacuum case: $\chi_m = 0$). For a ferromagnetic material there is a very large increase in self inductance.

On the other hand for diamagnetic/paramagnetic materials there is a small decrease/increase in the self-inductance.

For ferromagnetic materials the energy stored in an inductor increases by a large factor $\mu_r \approx 10^3 - 10^6$: See section 17.3 for energy stored in fields

17. 2. Electromagnetism with media: summary

Maxwell's equations in macroscopic form read

$$\underline{\nabla} \cdot \underline{D} = \rho_f \tag{1}$$

$$\underline{\nabla} \cdot \underline{B} = 0 \tag{2}$$

$$\underline{\nabla} \times \underline{\underline{E}} = -\frac{\partial \underline{\underline{B}}}{\partial t} \tag{3}$$

$$\underline{\nabla} \times \underline{H} = \underline{J}_f + \frac{\partial \underline{D}}{\partial t} \tag{4}$$

Definitions of $\underline{D}, \underline{H}$ are

$$\underline{D} = \epsilon_0 \underline{E} + \underline{P} \qquad \underline{B} = \mu_0 (\underline{H} + \underline{M}) \tag{5}$$

Relations for LIH Media

$$\underline{P} = \chi_E \epsilon_0 \underline{E} \qquad \underline{M} = \chi_m \underline{H} \tag{6}$$

$$\underline{D} = \epsilon_0 \epsilon_r \underline{E} \equiv \epsilon \underline{E} \qquad \underline{B} = \mu_0 \mu_r \underline{H} \equiv \mu \underline{H}$$
(7)

where $\epsilon_r = 1 + \chi_E$ $\mu_r = 1 + \chi_m$

17. 3. Energy densities and Poynting Vector

Recall that $\underline{E} \cdot \underline{J}_f$ is the power delivered per unit volume so the *energy density* u obeys

$$\frac{\mathrm{d}u}{\mathrm{d}t} = \underline{E} \cdot \underline{J}_f \tag{8}$$

Now use modified MIV to express

$$\underline{\underline{E}} \cdot \underline{J}_f = \underline{\underline{E}} \cdot (\underline{\nabla} \times \underline{\underline{H}}) - \underline{\underline{E}} \cdot \frac{\partial \underline{\underline{D}}}{\partial t}$$

Furthermore we can use a product rule from lecture 1 to write

$$\underline{\underline{E}} \cdot \underline{J} = \underline{\underline{H}} \cdot (\underline{\nabla} \times \underline{\underline{E}}) - \underline{\nabla} \cdot (\underline{\underline{E}} \times \underline{\underline{H}}) - \underline{\underline{E}} \cdot \frac{\partial \underline{\underline{D}}}{\partial t}$$
$$= -\underline{\underline{H}} \cdot \frac{\partial \underline{\underline{B}}}{\partial t} - \underline{\nabla} \cdot (\underline{\underline{E}} \times \underline{\underline{H}}) - \underline{\underline{E}} \cdot \frac{\partial \underline{\underline{D}}}{\partial t}$$
$$= -\frac{\partial}{\partial t} \left(\frac{1}{2} \underline{\underline{E}} \cdot \underline{\underline{D}} + \frac{1}{2} \underline{\underline{B}} \cdot \underline{\underline{H}} \right) - \underline{\nabla} \cdot (\underline{\underline{E}} \times \underline{\underline{H}})$$

provided that $\underline{E} \cdot \underline{\dot{D}} = \underline{\dot{E}} \cdot \underline{D}$ and $\underline{B} \cdot \underline{\dot{H}} = \underline{\dot{B}} \cdot \underline{H}$ which is true for linear static media. Then integrating over a volume V of the medium and using the divergence theorem on the second term as usual, we obtain from (8) for the total energy (c.f. section 14)

$$\frac{\mathrm{d}U}{\mathrm{d}t} = -\frac{\mathrm{d}}{\mathrm{d}t} \int_{V} \left(\frac{1}{2}\underline{E} \cdot \underline{D} + \frac{1}{2}\underline{B} \cdot \underline{H} \right) \mathrm{d}V - \oint_{S} (\underline{E} \times \underline{H}) \cdot \underline{\mathrm{d}S}$$
(9)

From the first term we identify the electric and magnetic energy densities as

$$u_M = \frac{1}{2}\underline{B} \cdot \underline{H} \qquad u_E = \frac{1}{2}\underline{E} \cdot \underline{D} \tag{10}$$

and from the second term we identify the Poynting vector as

$$\underline{S} = \underline{E} \times \underline{H} \tag{11}$$

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17. 4. Boundary Matching Problems

There are often have sharp interfaces between media. These boundaries acquire nonzero values of σ_P surface polarization charge and \underline{j}_{mag} surface magnetisation current

In keeping with use of MI-MIV in macroscopic form, we want to avoid considering these, and think about **free** charges and currents only ...

1. First condition (from $\underline{\nabla} \cdot \underline{D} = \rho_f$): Divergence theorem:

Figure 2: Gaussian surface for deriving continuity conditions on normal components (similar to Griffiths Fig 2.36)

$$\underline{\nabla} \cdot \underline{D} = \rho_f \qquad \Rightarrow \quad \oint \underline{D} \cdot \underline{\mathrm{d}S} = (Q_f)_{enclosed}$$

Apply to small pillbox or "patch", vector area $\underline{dS} = \hat{\underline{n}} dS$

$$(\underline{D}_2 - \underline{D}_1) \cdot \underline{\hat{n}} \, \mathrm{d}S = \sigma_f \, \mathrm{d}S$$

surface density of FREE charges only. In the absence of free surface charges D_{normal} is continuous. We can also write this as

$$(\underline{D}_2 - \underline{D}_1) \cdot \underline{\hat{n}} = \sigma_f$$

2. Second condition (from $\underline{\nabla} \cdot \underline{B} = 0$):

$$\underline{\nabla} \cdot \underline{B} = 0 \qquad \Rightarrow \qquad \int \underline{B} \cdot \underline{\mathrm{d}} S = 0$$

Apply to small Gaussian pill box (or "patch")

$$\int \underline{B} \cdot \underline{\mathrm{d}}S = (\underline{B}_2 - \underline{B}_1) \cdot \underline{\hat{n}} \, \mathrm{d}S = 0$$

Therefore B_{normal} is continuous. This is completely general.

3. Third condition (from $\nabla \times \underline{E} = -\partial \underline{B}/\partial t$): $\underline{\hat{t}} =$ unit tangent satisfies $\underline{\hat{t}} \cdot \underline{\hat{n}} = 0$; we take a rectangular loop straddling the interface length ℓ height h

$$\oint \underline{E} \cdot \underline{dl} = (\underline{E}_1 - \underline{E}_2) \cdot \hat{\underline{t}} \, l \qquad = -\frac{\partial}{\partial t} \Phi_B$$

Unless <u>B</u> is infinite, the magnetic flux cutting the loop $\Phi_B \to 0$ as $h \to 0$

$$\Rightarrow (\underline{E}_1 - \underline{E}_2) \cdot \underline{\hat{t}} = 0$$

Figure 3: Amperian loop for deriving continuity conditions on tangential components (similar to Griffiths Fig 2.37)

but $\underline{\hat{t}}$ is arbitrary within plane of the surface: $\underline{E}_{tangential}$ is continuous is completely general as it stands. **N.B.** this is **two** conditions in 3D

4. Fourth condition $(\underline{\nabla} \times \underline{H} = \underline{J}_f + \partial \underline{D} / \partial t)$:

 $\underline{j}_f = \mathrm{free} \ \mathrm{surface} \ \mathrm{current} \ / \ \mathrm{unit} \ \mathrm{area}$

$$\oint \underline{H} \cdot \underline{\mathrm{d}} l = \underline{j}_f \cdot \underline{\hat{s}} \, \ell + \frac{\partial \underline{D}}{\partial t} \cdot \underline{\hat{s}} \, \ell \, h$$

where $\underline{\hat{s}} = \underline{\hat{t}} \times \underline{\hat{n}} =$ unit vector \perp to Ampèrian loop Now take $h \rightarrow 0$: last term vanishes

$$\oint \underline{H} \cdot \underline{dl} = (\underline{H}_1 - \underline{H}_2) \cdot \hat{\underline{t}} \,\ell = \underline{j}_f \cdot \hat{\underline{s}} \,\ell$$

In the absence of free surface currents $\underline{H}_{tangential}$ is continuous

The general form is rarely needed and may be written in several equivalent ways:

$$\begin{array}{rcl} (\underline{H}_1 - \underline{H}_2) \cdot \underline{\hat{t}} &=& \underline{j}_f \cdot \underline{\hat{s}} \\ (\underline{H}_2^{tang} - \underline{H}_1^{tang}) &=& \underline{j}_f \times \underline{\hat{n}} \\ (\underline{H}_2 - \underline{H}_1) \times \underline{\hat{n}} &=& -\underline{j}_f \end{array}$$

Summary of the continuity conditions

| 1. | D_n | continuous | if $\sigma_f = 0$ |
|----|-------------------|------------|--------------------------------------|
| 2. | B_n | continuous | always |
| 3. | \underline{E}_t | continuous | always |
| 4. | \underline{H}_t | continuous | if $\underline{j}_f = \underline{0}$ |

These are key results and you should know the derivations.

Problems with nonzero σ_f or \underline{j}_f are uncommon but for these:

$$(\underline{D}_2 - \underline{D}_1) \cdot \underline{\hat{n}} = \sigma_f$$
 replaces 1

$$(\underline{H}_2^{tang} - \underline{H}_1^{tang}) = \underline{j}_f \times \underline{\hat{n}}$$
 replaces 4