

Electromagnetism - Lecture 16

Waveguides & Cavities

- Waves between Parallel Plates
- TE and TM Modes
- Rectangular Waveguides
- The TE₀₁ Mode
- Power Transmission
- RF Cavities

Waves between Parallel Plates

Two infinite parallel conducting plates in the x/z plane are separated by a distance $y = b$

A wave incident on a plate at an angle θ in the y/z plane is reflected and bounces back and forth between the plates

Waves propagate between the plates in the z direction

T(ransverse) **E**(lectric) modes have \mathbf{E}_x and \mathbf{B} in the y/z plane

T(ransverse) **M**(agnetic) modes have \mathbf{B}_x and \mathbf{E} in the y/z plane

TEM modes have \mathbf{B}_x and \mathbf{E}_y , and propagate along z only at $\theta = 90^\circ$, i.e. they don't bounce off the walls

TE modes between Plates

Electric field is *parallel* to the plates in the \mathbf{x} direction!

Incident plane wave: $E_I = E_0 e^{i(\omega t - kz \cos \theta + ky \sin \theta)}$

Reflected plane wave: $E_R = -E_0 e^{i(\omega t - kz \cos \theta - ky \sin \theta)}$

$$E_x = E_I + E_R = E_0 e^{i(\omega t - kz \cos \theta)} (e^{iky \sin \theta} - e^{-iky \sin \theta})$$

$$E_x = 2i \sin(ky \sin \theta) E_0 e^{i(\omega t - kz \cos \theta)}$$

Boundary condition at plates is $E_{||} = 0$

$E_x = 0$ at $y = 0$ and $y = b$ is satisfied if $kb \sin \theta = n\pi$

where n is an integer known as the **mode number**

Notes:

Diagrams:

Fields of TE modes

We write the fields in terms of the mode number n and the *effective wavenumber* $k' = k \cos \theta$ where $kb \sin \theta = n\pi$

$$E_x = 2i \sin\left(\frac{n\pi y}{b}\right) E_0 e^{i(\omega t - k' z)}$$

From M3:

$$\frac{\partial B_y}{\partial t} = -\frac{\partial E_x}{\partial z} \quad \frac{\partial B_z}{\partial t} = \frac{\partial E_x}{\partial y}$$

$$B_y = 2i \frac{k'}{\omega} \sin\left(\frac{n\pi y}{b}\right) E_0 e^{i(\omega t - k' z)}$$

$$B_z = 2 \frac{\sqrt{k^2 - k'^2}}{\omega} \cos\left(\frac{n\pi y}{b}\right) E_0 e^{i(\omega t - k' z)}$$

Boundary conditions on magnetic field at plates:

$B_{\perp} = 0$ is satisfied by B_y for $y = 0$ and $y = b$

$H_{\parallel} = \mathbf{J}$ from B_z requires oscillating surface currents at the plates

Fields of TM modes

Magnetic field is *parallel* to the plates in the \mathbf{x} direction!

$$B_x = B_0 \cos\left(\frac{n\pi y}{b}\right) e^{i(\omega t - k'z)} \quad kb \sin \theta = n\pi$$

The mode numbers are the same as for the TE modes!

From M4 the electric field components can be derived:

$$E_y = B_0 \frac{\omega k'}{k^2} \cos\left(\frac{n\pi y}{b}\right) e^{i(\omega t - k'z)}$$

$$E_z = iB_0 \frac{\omega \sqrt{(k^2 - k'^2)}}{k^2} \sin\left(\frac{n\pi y}{b}\right) e^{i(\omega t - k'z)}$$

Boundary conditions on fields at plates:

$H_{\parallel} = \mathbf{J}$ from B_x requires oscillating surface currents at the plates

$E_{\parallel} = 0$ is satisfied by E_z for $y = 0$ and $y = b$

$D_{\perp} = \rho$ from E_y requires oscillating surface charges at the plates

Notes:

Diagrams:

Notes:

Diagrams:

Rectangular Waveguides

Formed by pairs of parallel conducting plates in the y/z and x/z planes with separations $x = a$ and $y = b$ ($a < b$ by convention)

Waves still propagate in the z direction by bouncing off plates

TE modes have E_x and E_y but no E_z

TM modes have B_x and B_y but no B_z

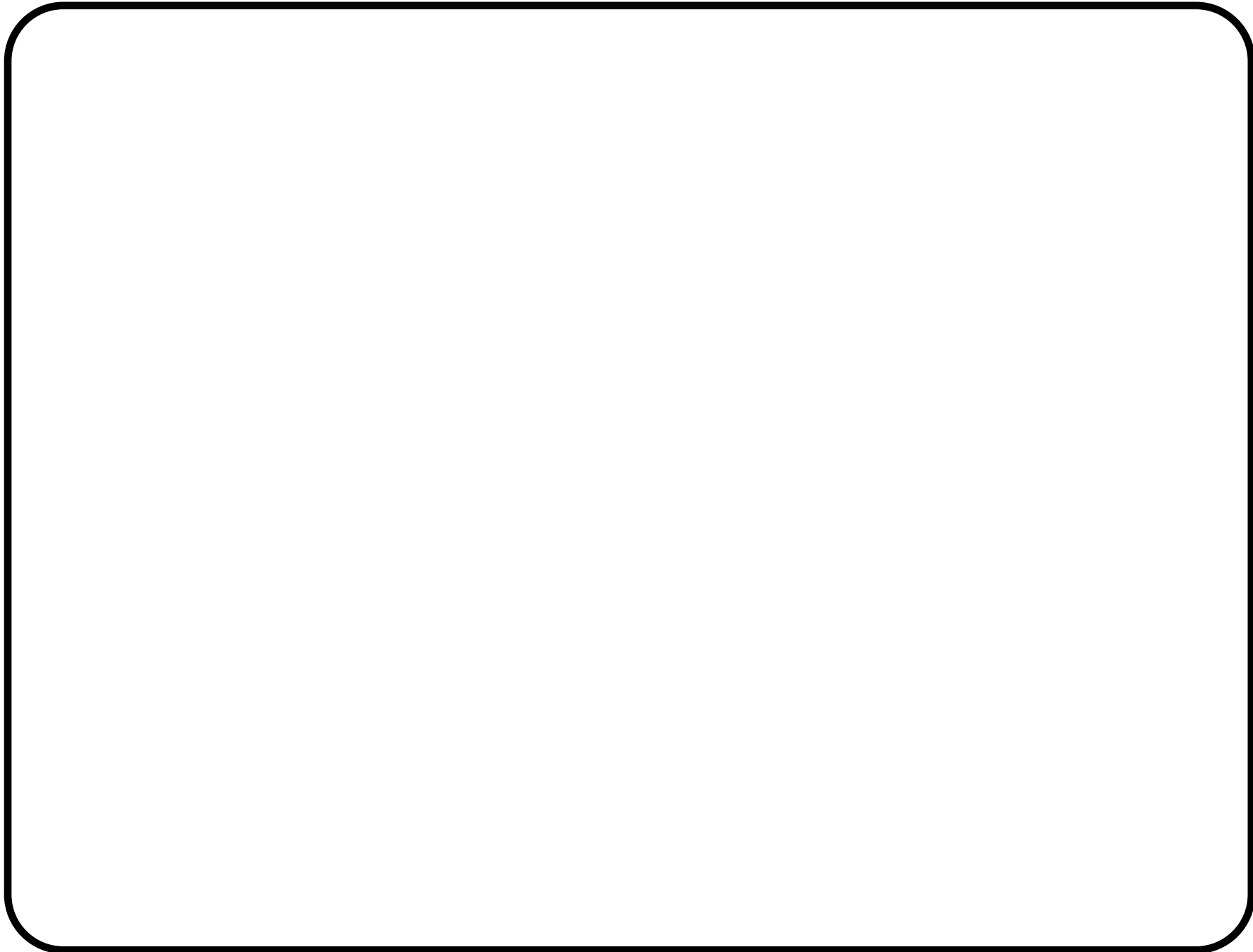
TEM modes with no E_z or B_z do not satisfy boundary conditions!

TE and **TM** modes have *two* mode numbers m and n and an effective wavenumber k' :

$$k' = \sqrt{\left(k^2 - \frac{m^2\pi^2}{a^2} - \frac{n^2\pi^2}{b^2}\right)}$$

There is a cutoff frequency ν_{min} for each mode:

$$k^2 > \left(\frac{m^2\pi^2}{a^2} + \frac{n^2\pi^2}{b^2}\right) \quad \nu_{min} = \frac{c}{2} \sqrt{\frac{m^2}{a^2} + \frac{n^2}{b^2}}$$



Fields of TE modes in Waveguides

Extrapolating from what we found for one set of parallel plates:

$$E_x = -\frac{Cn\pi}{b} \cos\left(\frac{m\pi x}{a}\right) \sin\left(\frac{n\pi y}{b}\right) e^{i(\omega t - k'z)}$$

$$E_y = \frac{Cm\pi}{a} \sin\left(\frac{m\pi x}{a}\right) \cos\left(\frac{n\pi y}{b}\right) e^{i(\omega t - k'z)}$$

$$B_x = -\frac{k'}{\omega} \frac{Cm\pi}{a} \sin\left(\frac{m\pi x}{a}\right) \cos\left(\frac{n\pi y}{b}\right) e^{i(\omega t - k'z)}$$

$$B_y = -\frac{k'}{\omega} \frac{Cn\pi}{b} \cos\left(\frac{m\pi x}{a}\right) \sin\left(\frac{n\pi y}{b}\right) e^{i(\omega t - k'z)}$$

$$B_z = i \frac{(k^2 - k'^2)}{\omega} C \cos\left(\frac{m\pi x}{a}\right) \cos\left(\frac{n\pi y}{b}\right) e^{i(\omega t - k'z)}$$

where C is a constant related to the amplitude

The TE01 mode of a Waveguide

The highest effective wavenumber has $m = 0, n = 1$ where $a < b$

The TE01 mode with $m = 0, n = 1$ has the lowest cutoff ν_{min}

There is no TM01 mode!

$m = 0$ or $n = 0$ do not satisfy boundary conditions.

The lowest TM mode is TM11.

Can choose ν and b so that TE01 is the only mode allowed.

The TE01 mode of rectangular waveguides is widely used for routing electromagnetic waves

Optical fibres can be treated as circular waveguides

For a discussion see Jackson Pp.378-389

Fields of TE₀₁ mode

Setting $m = 0$, $n = 1$ in the field expressions:

$$E_x = -\frac{C\pi}{b} \sin\left(\frac{\pi y}{b}\right) e^{i(\omega t - k'z)}$$

$$B_y = -\frac{k'}{\omega} \frac{C\pi}{b} \sin\left(\frac{\pi y}{b}\right) e^{i(\omega t - k'z)}$$

$$B_z = i \frac{(k^2 - k'^2)}{\omega} C \cos\left(\frac{\pi y}{b}\right) e^{i(\omega t - k'z)}$$

The other field components B_x , E_y , E_z are zero

Boundary conditions on fields at plates:

$E_{\parallel} = 0$ is satisfied by E_x for $y = 0$ and $y = b$

$B_{\perp} = 0$ is satisfied by B_y for $y = 0$ and $y = b$

$H_{\parallel} = \mathbf{J}$ surface currents from B_z and B_y at the y/z plates

For pictures of these see Pp.422-423 of Grant & Philips

Notes:

Diagrams:

Power transmission in a Waveguide

Power transmission is given by time-averaged Poynting vector

For the TE₀₁ mode:

$$\langle N_z \rangle = \langle E_x H_y \rangle = \frac{k'}{2\mu_0\omega} E_0^2 \sin^2\left(\frac{\pi y}{b}\right)$$

The other time-averaged components $\langle N_x \rangle$ and $\langle N_y \rangle$ are zero

The total power over the waveguide cross-section is:

$$P_z = \int_0^b \langle N_z \rangle dy \int_0^a dx = \frac{abk'}{2\pi\mu_0\omega} E_0^2 \int_0^\pi \sin^2 \theta d\theta$$

$$P_z = \frac{abk'}{4\mu_0\omega} E_0^2 = \frac{A}{4\mu_0 v_P} E_0^2$$

The total power is proportional to $A = ab$, the cross-sectional area and inversely proportional to $v_P = \omega/k'$, the effective phase velocity

RF Cavities

A rectangular box is formed by three pairs of parallel conducting plates with separations $x = a$, $y = b$ and $z = d$ ($d < a < b$)

Standing waves can be excited in the box

The waves do not propagate in any direction!

TE modes have E_x and E_y but no E_z (lowest mode TE₀₁₁)

TM modes have B_x and B_y but no B_z (lowest mode TM₁₁₁)

TE and **TM** modes have *three* mode numbers l , m and n

The resonant frequencies of the cavity ω are:

$$\frac{\omega}{c} = k = \sqrt{\frac{l^2 \pi^2}{d^2} + \frac{m^2 \pi^2}{a^2} + \frac{n^2 \pi^2}{b^2}}$$

Oscillating fields in RF cavities are used to accelerate charges