

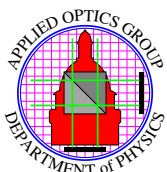


## Topic 3: Operation of Simple Lens

**Aim:** Covers imaging of simple lens using Fresnel Diffraction, resolution limits and basics of aberrations theory.

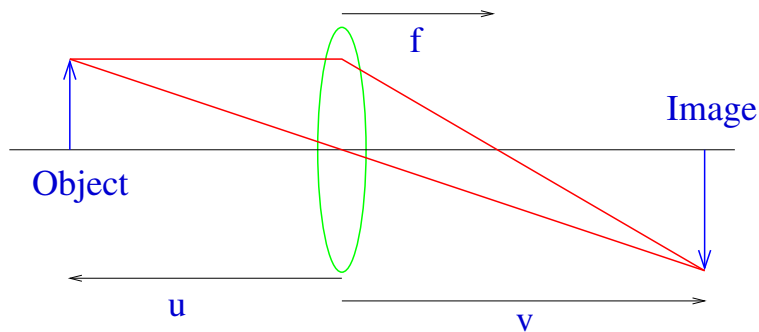
**Contents:**

1. Phase and Pupil Functions of a lens
2. Image of Axial Point
3. Example of Round Lens
4. Diffraction limit of lens
5. Defocus
6. The Strehl Limit
7. Other Aberrations



# Ray Model

Simple Ray Optics gives



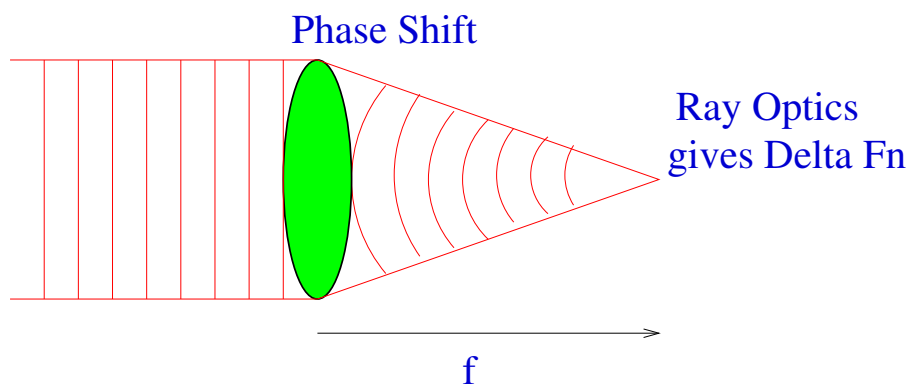
Imaging properties of

$$\frac{1}{u} + \frac{1}{v} = \frac{1}{f}$$

The focal length is given by

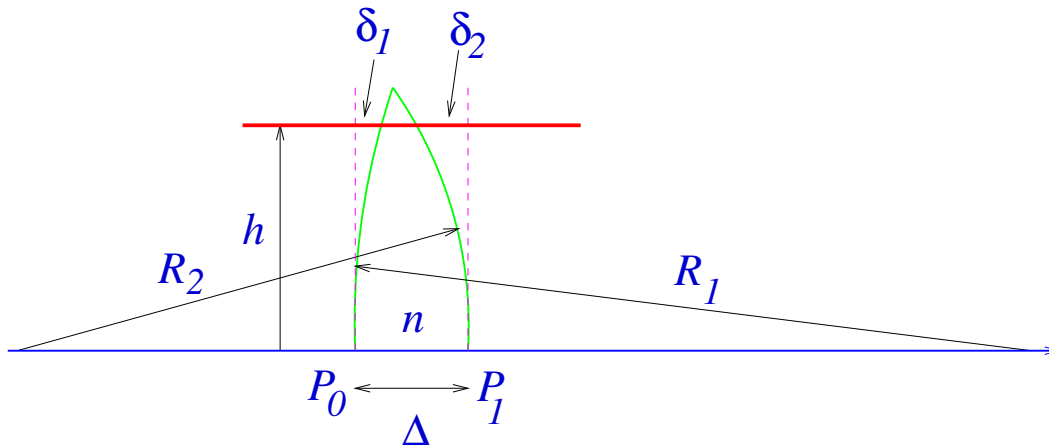
$$\frac{1}{f} = (n - 1) \left[ \frac{1}{R_1} + \frac{1}{R_2} \right]$$

For Infinite object



Lens introduces a path length difference, or **PHASE SHIFT**.

## Phase Function of a Lens



With **NO** lens, Phase Shift between ,  $P_0 \rightarrow P_1$  is

$$\Phi = \kappa \Delta \quad \text{where } \kappa = \frac{2\pi}{\lambda}$$

with lens in place, at distance  $h$  from optical,

$$\Phi = \kappa \left( \underbrace{\delta_1 + \delta_2}_{\text{Air}} + n \underbrace{(\Delta - \delta_1 - \delta_2)}_{\text{Glass}} \right)$$

which can be arranged to give

$$\Phi = \kappa n \Delta - \kappa (n - 1) (\delta_1 + \delta_2)$$

where  $\delta_1$  and  $\delta_2$  depend on  $h$ , the ray height.

## Parabolic Approximation

Lens surfaces are **Spherical**, but:

If  $R_1$  &  $R_2 \gg h$ , take parabolic approximation

$$\delta_1 = \frac{h^2}{2R_1} \quad \text{and} \quad \delta_2 = \frac{h^2}{2R_2}$$

So that

$$\Phi(h) = \kappa\Delta n + \frac{\kappa h^2}{2}(n-1) \left( \frac{1}{R_1} + \frac{1}{R_2} \right)$$

substituting for focal length, we get

$$\Phi(h) = \kappa\Delta n - \frac{\kappa h^2}{2f}$$

So in 2-dimensions,  $h^2 = x^2 + y^2$ , so that

$$\Phi(x, y; f) = \kappa\Delta n - \kappa \frac{(x^2 + y^2)}{2f}$$

the phase function of the lens.

**Note:** In many cases  $\kappa\Delta n$  can be ignored since absolute phase not usually important.

The difference between Parabolic and Spherical surfaces will be considered in the next lecture.



## Pupil Function

The pupil function is used to define the physical size and shape of the lens.

$p(x,y) \Rightarrow$  Shape of lens

so the total effect of the lens of focal length is

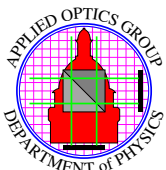
$$p(x,y) \exp(i\Phi(x,y;f))$$

For a circular lens of radius  $a$ ,

$$\begin{aligned} p(x,y) &= 1 \quad \text{if } x^2 + y^2 \leq a^2 \\ &= 0 \quad \text{else} \end{aligned}$$

The circular lens is the most common, but all the following results apply equally well for other shapes.

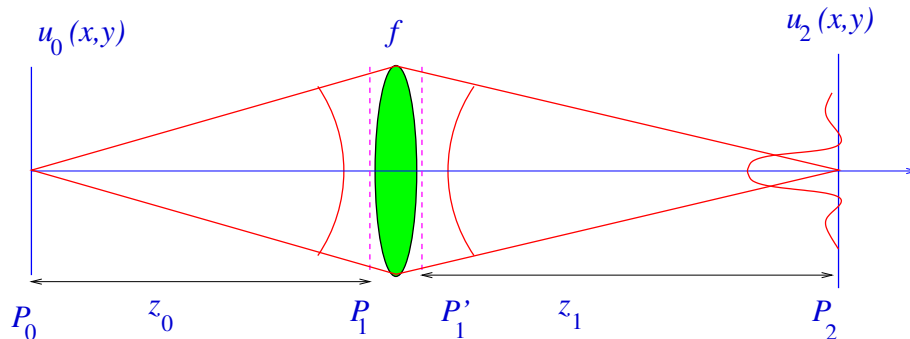
Pupil Function of a simple lens is real and positive, but it will be used later to include aberrations, and will become complex.



## Fresnel Image of Axial Point

We will now consider the imaging of an axial point using the Fresnel propagation equations from the last lecture.

Consider the system.



In plane  $P_0$  we have that

$$u_0(x, y) = A_0 \delta(x, y)$$

so in plane  $P_1$  a distance  $z_0$ , we have that,

$$\begin{aligned} u(x, y; z_0) &= h(x, y; z_0) \odot A_0 \delta(x, y) \\ &= A_0 h(x, y; z_0) \end{aligned}$$

where  $h(x, y; z)$  is the free space impulse response function.

If we now assume that the lens is **thin**, then there is no diffraction between planes,  $P_1$  and  $P_1'$ , so in  $P_1'$  we have

$$u'(x, y; z_0) = A_0 h(x, y; z_0) p(x, y) \exp(i\Phi(x, y; f))$$

so finally in  $P_2$  a further distance  $z_1$  we have that

$$\begin{aligned} u_2(x, y) &= u'(x, y; z_0) \odot h(x, y; z_1) \\ &= A_0 h(x, y; z_0) p(x, y) \exp(i\Phi(x, y; f)) \odot h(x, y; z_1) \end{aligned}$$



Take the Fresnel approximation, where

$$h(x, y; z) = \frac{\exp(i\kappa z)}{i\lambda z} \exp\left(i\frac{\kappa}{2z}(x^2 + y^2)\right)$$

and

$$\Phi(x, y; f) = \kappa n\Delta - \frac{\kappa}{2f}(x^2 + y^2)$$

so we get that

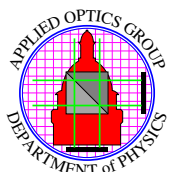
$$u(x, y; z_0) = \frac{A_0 \exp(i\kappa z_0)}{i\lambda z_0} \exp\left(i\frac{\kappa}{2z_0}(x^2 + y^2)\right)$$

then by more substitution,

$$u'(x, y; z_0) = \frac{A_0 \exp(i\kappa(z_0 + n\Delta))}{i\lambda z_0} p(x, y) \exp\left(i\frac{\kappa}{2}\left(\frac{1}{z_0} - \frac{1}{f}\right)(x^2 + y^2)\right)$$

Finally!, we can substitute and expand to get

$$u_2(x, y) = \underbrace{\frac{A_0}{\lambda^2 z_0 z_1} \exp(i\kappa(z_0 + z_1 + n\Delta))}_1 \underbrace{\exp\left(i\frac{\kappa}{2z_1}(x^2 + y^2)\right)}_2 \underbrace{\iint p(s, t) \exp\left(i\frac{\kappa}{2}(s^2 + t^2) \left(\frac{1}{z_0} + \frac{1}{z_1} - \frac{1}{f}\right)\right)}_3 \underbrace{\exp\left(-i\frac{\kappa}{z_1}(sx + ty)\right) ds dt}_4$$





Look at the term:

1. Constant, amplitude gives absolute brightness, phase not measurable.
2. Quadratic phase term in plane  $P_2$ , no effect on intensity, and usually ignored.
3. Quadratic phase term across the Pupil, depends on both  $z_0$  and  $z_1$ .
4. Scaled Fourier Transform of Pupil Function.

If we select the location of plane  $P_2$  such that

$$\frac{1}{z_0} + \frac{1}{z_1} - \frac{1}{f} = 0$$

Note same expression as Ray Optics, then we can write

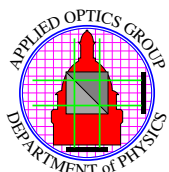
$$u_2(x, y) = B_0 \exp\left(i \frac{\kappa}{2z_1}(x^2 + y^2)\right) \iint p(s, t) \exp\left(-i \frac{\kappa}{z_1}(sx + ty)\right) ds dt$$

so in plane  $P_2$  we have the scaled Fourier Transform of the Pupil Function, (plus phase term).

Intensity in plane  $P_2$  is thus

$$g(x, y) = |u_2(x, y)|^2 = B_0^2 \left| \iint p(s, t) \exp\left(-i \frac{\kappa}{z_1}(sx + ty)\right) ds dt \right|^2$$

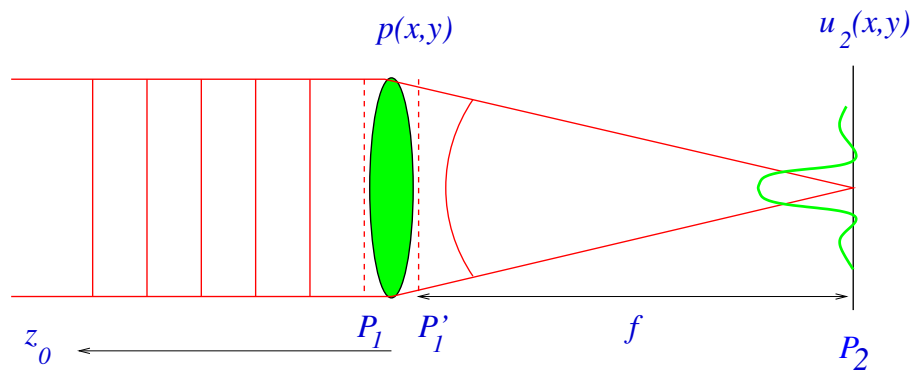
Being the scaled power spectrum of the Pupil Function.





## Image of a Distant Object

For a distant object  $z_0 \rightarrow \infty$  and  $z_1 \rightarrow f$



Then the amplitude in  $P_2$  becomes,

$$u_2(x,y) = B_0 \exp\left(i\frac{\kappa}{2f}(x^2 + y^2)\right) \iint p(s,t) \exp\left(-i\frac{\kappa}{f}(sx + ty)\right) dsdt$$

which being the scaled Fourier Transform of the Pupil function.

The intensity is therefore:

$$g(x,y) = B_0^2 \left| \iint p(s,t) \exp\left(-i\frac{\kappa}{f}(sx + ty)\right) dsdt \right|^2$$

which is known as the **Point Spread Function** of the lens

### Key Result

**Note on Units:**  $x, y, s, t$  all have units of length  $m$ . Scaler Fourier kernel is:

$$\exp\left(-i\frac{2\pi}{\lambda f}(sx + ty)\right)$$

## Simple Round Lens

Consider the case of round lens of radius  $a$ , amplitude in  $P_2$  then becomes,

$$u_2(x, y) = \hat{B}_0 \iint_{s^2+t^2 \leq a^2} \exp\left(-i\frac{\kappa}{f}(sx + ty)\right) ds dt$$

the external phase term has been absorbed into  $\hat{B}_0$

This can be integrated, using standard results (see Physics 3 Optics notes or tutorial solution), to give:

$$u_2(x, 0) = 2\pi\hat{B}_0 a^2 \frac{J_1\left(\frac{\kappa a}{f}x\right)}{\frac{\kappa a}{f}x}$$

where  $J_1$  is the first order Bessel Function.

This is normally normalised so that  $u_2(0, 0) = 1$ , and noting that the output is circularly symmetric, we get that,

$$u_2(x, y) = 2 \frac{J_1\left(\frac{\kappa a}{f}r\right)}{\frac{\kappa a}{f}r}$$

where  $x^2 + y^2 = r^2$ .

The intensity PSF is then given by,

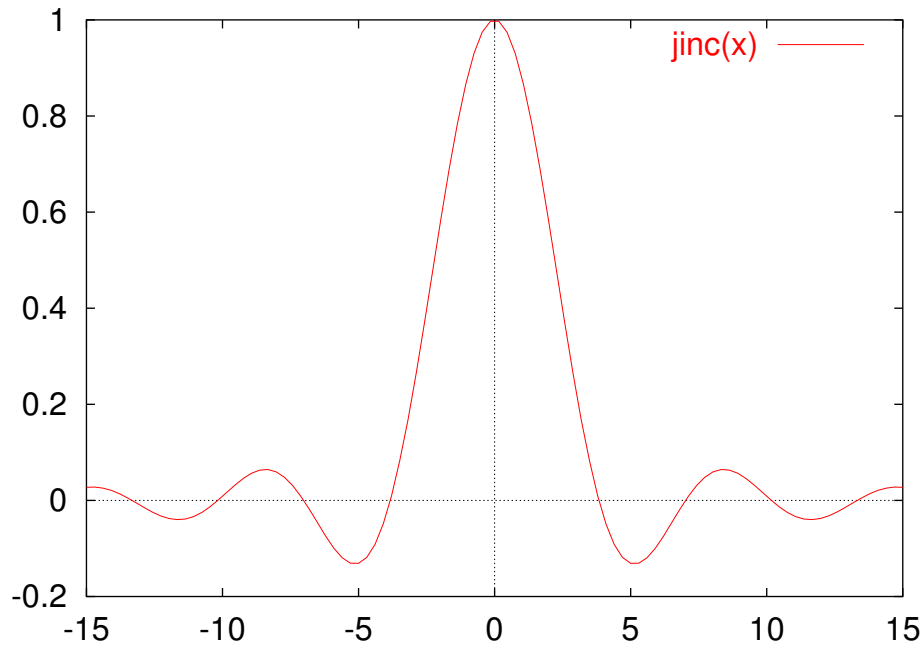
$$g(x, y) = 4 \left| \frac{J_1\left(\frac{\kappa a}{f}r\right)}{\frac{\kappa a}{f}r} \right|^2$$

which is known as the **Airy Distribution**, first derived in 1835.

# Shape of jinc

The function

$$\text{jinc}(x) = \frac{2J_1(x)}{x}$$



Similar shape to the  $\text{sinc}()$  function, except

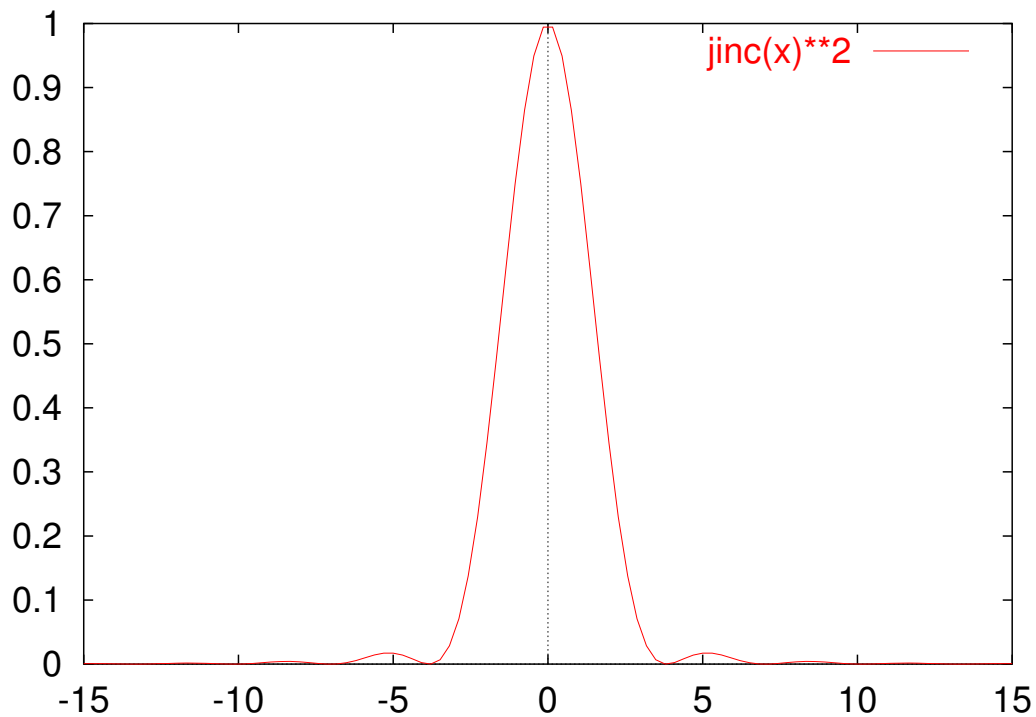
- Zeros at different locations.
- Lower secondary maximas

Zeros of  $\text{jinc}()$  located at

$x_0$	3.832	$1.22\pi$
$x_0$	7.016	$2.23\pi$
$x_0$	10.174	$3.24\pi$
$x_0$	13.324	$4.24\pi$

## Shape of $\text{jinc}^2()$

The PSF function is the square of the  $\text{jinc}()$ ,



We get 88% of power in the central peak.

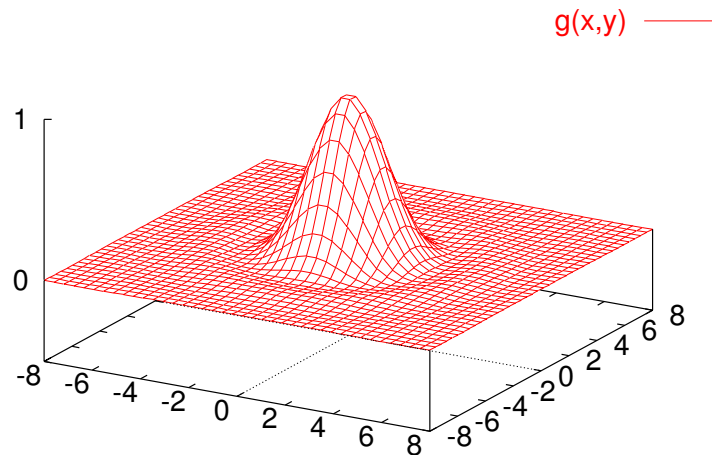
Height of secondary maximas

Order	Location	Height
1	5.136	0.0175
2	8.417	0.0042
3	11.620	0.0016

## Shape of PSF

The PSF is circular symmetry, being

$$g(x,y) = \text{jinc}^2\left(\frac{\kappa a}{f}r\right)$$



Radius of first zero occurs at

$$\frac{\kappa a}{f}r_0 = 1.22\pi \quad \Rightarrow \quad r_0 = \frac{0.61\lambda f}{a}$$

**Define:**  $F_{No}$  as

$$F_{No} = \frac{f}{2a} = \frac{\text{Focal Length}}{\text{Diameter}}$$

Then the zero of the PSF occur at

$$r_0 = 1.22\lambda F_{No}$$

$$r_1 = 2.23\lambda F_{No}$$

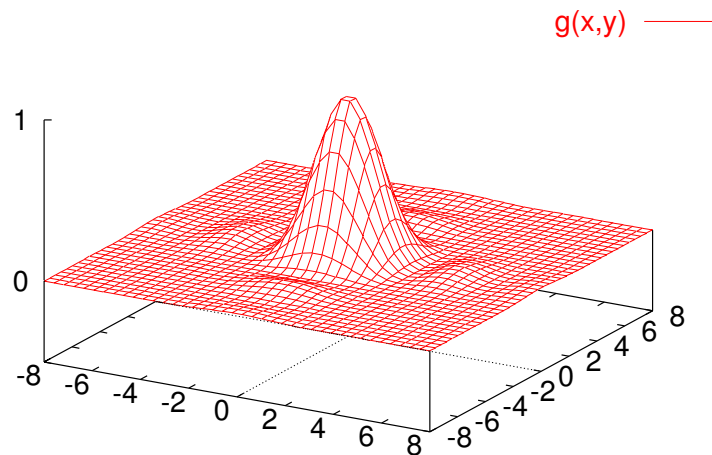
$$r_2 = 3.24\lambda F_{No}$$

All lenses with the same  $F_{No}$  have the same Point Spread Function.

## Other Shaped Lenses

This method of calculating the PSF is valid for any Pupil Function, for example a “square” lens of size  $2a \times 2a$  will have a PSF

$$g(x,y) = \text{sinc}^2\left(\frac{\kappa a}{f}x\right) \text{sinc}^2\left(\frac{\kappa a}{f}y\right)$$



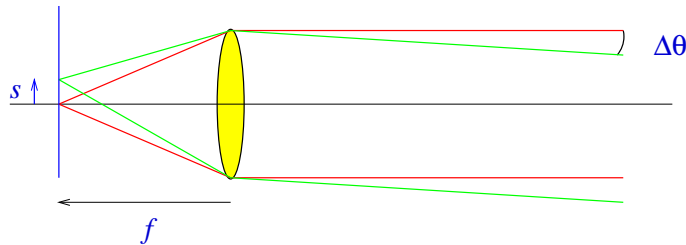
with the first zeros in the  $x$  direction at:

$$\frac{\kappa a}{f}x_0 = \pi \quad \Rightarrow \quad x_0 = \frac{0.5\lambda f}{a}$$

See tutorial questions for important case of annular lens and lens with Gaussian transmission function.

## Diffraction Limit of Lens

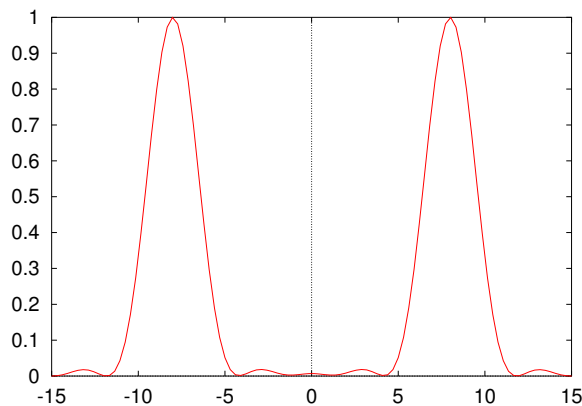
**Angular Resolution:** Take two point sources (stars) at infinity separated by  $\Delta\theta$



$$s = f \tan \Delta\theta \approx f \Delta\theta \quad \text{Small } \Delta\theta$$

For *large*  $\Delta\theta$ , then

$$s \gg r_0 \quad \text{Width of PSF}$$



Then two stars resolved.

While is

$$\Delta\theta f \ll r_0 \quad \text{See one star}$$

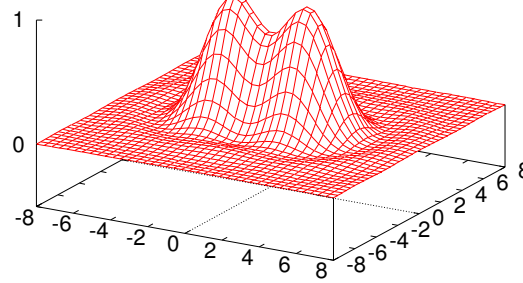
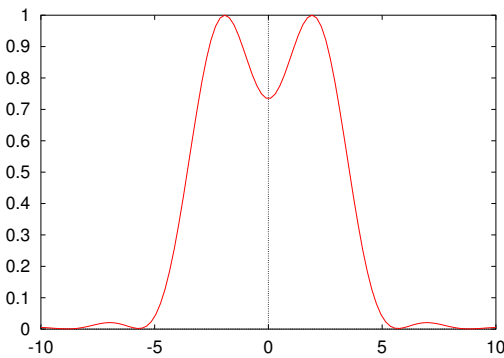
Then star NOT resolved.

Note: Light from two distant stars, so Intensities will sum.

## Rayleigh Limit

Limit when start “just” resolved. For stars of equal brightness, when

$$s = r_0 \rightarrow 27\% \text{ “Dip” between peaks}$$



Stars are said to be “just” resolved.

$$\Delta\theta_0 f = r_0 = \frac{0.61\lambda f}{a}$$

giving that

$$\Delta\theta_0 = \frac{0.61\lambda}{a} = \frac{1.22\lambda}{d}$$

So angular resolution limit of a lens depend **ONLY** on it diameter.

### Key Result

See tutorial questions for other configurations and lenses with different Pupil Functions.





## Examples

**Telescope:** Medium size,

$$d = 10\text{cm} \quad \& \quad \lambda = 550\text{nm} \quad \text{Green}$$

Then resolution limit

$$\Delta\theta_0 = 6.71 \times 10^{-6}\text{Rad} = 1.4'' \text{ of arc}$$

**Human Eye:** in normal sunlight

$$d = 2\text{mm} \quad \& \quad \lambda = 550\text{nm}$$

Then resolution limit

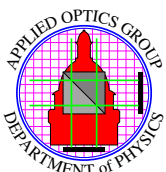
$$\Delta\theta = 3.3 \times 10^{-4}\text{Rad} \approx 1' \text{ of arc}$$

Actual resolution limit of eye is really limited by the spacing of cones on the retina, and is typically  $5 \times 10^{-4}\text{Rad}$  (1 mm divisions on a ruler just resolved at 2 m).

### Rule of Thumb

- Resolution of eye  $1' \rightarrow 2'$  of arc.
- Resolution of telescope  $1''$  of arc.

**Aside:** For all telescopes bigger than 10 cm resolution limited by atmospheric movement, so resolution of  $1''$  of arc is true for all optical earth bound telescopes.



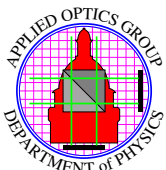


## Angular Measures

Many systems still specified in degrees, and fractions of degrees

$$\begin{aligned}1^\circ &= \frac{2\pi}{360}\text{Rad} = 0.0174\text{Rad} \\1' &= \frac{1}{60}^\circ = 2.91 \times 10^{-4}\text{Rad} \\1'' &= \frac{1}{60}' = 4.85 \times 10^{-6}\text{Rad}\end{aligned}$$

These measure are still in use on spectrometers, telescopes, astronomical tables and maps and charts.



## Defocus of Optical System

Consider point source imaged by a lens

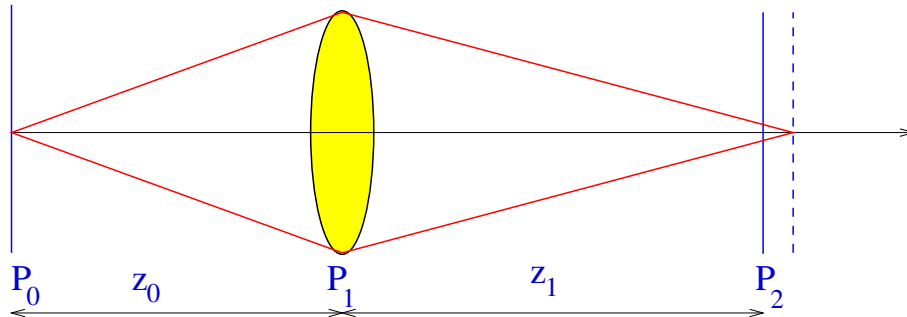


Image is “In Focus” if

$$\frac{1}{z_0} + \frac{1}{z_1} = \frac{1}{f}$$

Move  $P_2$  system is “Defocused”.

Define **Defocus Parameter**,  $D$  as:

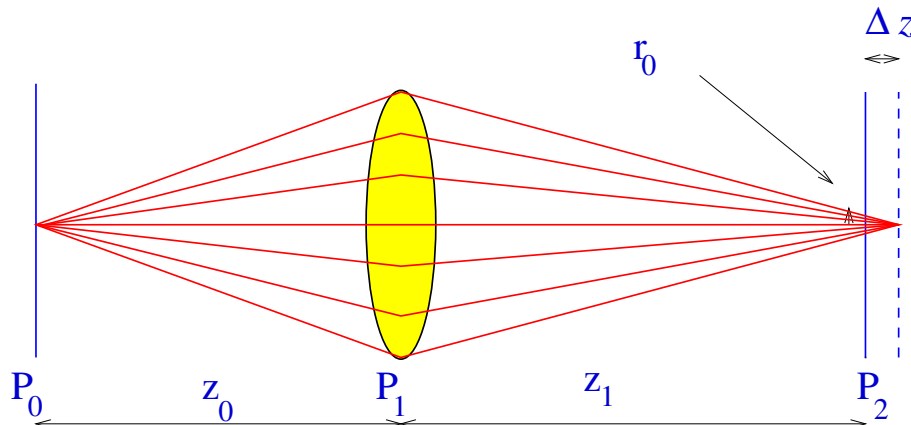
$$D = \frac{1}{z_0} + \frac{1}{z_1} - \frac{1}{f}$$

Then if

$D < 0$  Negative Defocus, ( $z_1$  too large)

$D > 0$  Positive Defocus, ( $z_1$  too small)

**Ray Optics:** Defocus system by  $\Delta z$



Radius of the spot is given by similar triangles to be

$$r_0 = \frac{\Delta z d}{2z_1}$$

where the lens is of diameter  $d$ . So larger defocus, large PSF. OK for **Large Defocus**

**Scalar Theory:** From previous, if  $D \neq 0$ , then in  $P_2$ ,

$$u_2(x, y) = \hat{B}_0 \iint \overbrace{p(s, t) \exp\left(i\frac{\kappa}{2}D(s^2 + t^2)\right)}^{\text{Effective Pupil Function}} \exp\left(-i\frac{\kappa}{z_1}(sx + ty)\right) ds dt$$

Which is the Fourier Transform of the “Effective Pupil Function”,

$$q(x, y) = p(x, y) \exp\left(i\frac{\kappa}{2}D(x^2 + y^2)\right)$$

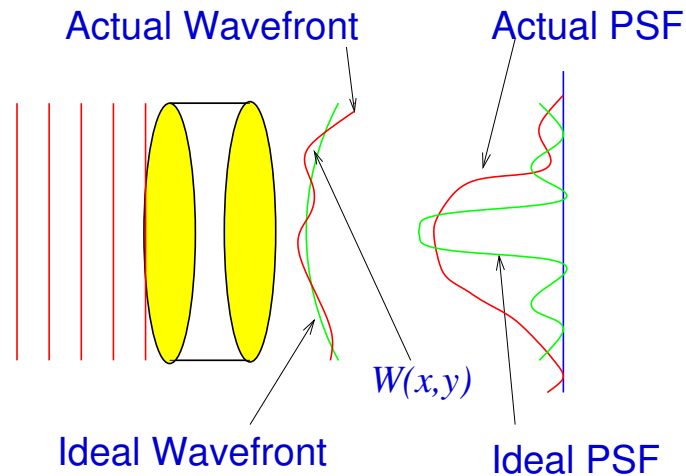
Pupil function goes complex under defocus.

**Note:** Pupil function is product so PSF is a convolution, which will be “wider” than ideal focus.

## Wavefront Aberration

To get ideal PSF (sharp focus), we need **Parabolic Wave** front behind the lens.

Actual wavefront may vary from this ideal.



**Define Wavefront Aberration Function** as deviation from ideal parabolic wavefront.

System Pupil Function then becomes,

$$q(x, y) = p(x, y) \exp(i\kappa W(x, y))$$

where

$W(u, v)$  is **Wavefront Aberration Function**

The Effective Pupil Function is now Complex, with the PSF given by

$$g(x, y) = B_0^2 \left| \iint q(s, t) \exp\left(-i\frac{\kappa}{z_1}(sx + ty)\right) ds dt \right|^2$$

This is a general method of dealing with all types of aberrations.

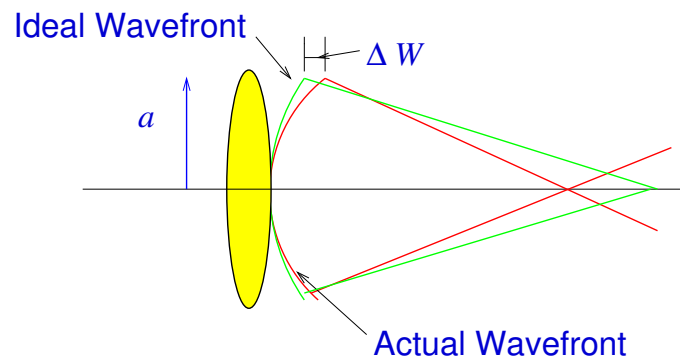
## Defocus as an Aberration

Under defocus, the wavefront aberration is

$$W(x, y) = \frac{D}{2}(x^2 + y^2)$$

Measure the Defocus as the extent of the wavefront aberration at the edge of the lens, at

$$x^2 + y^2 = a^2$$



Denote wavefront aberration at edge by  $\Delta W$ , so wavefront aberration is:

$$W(x, y) = \Delta W \left( \frac{x^2 + y^2}{a^2} \right)$$

so

$$D = \frac{2\Delta W}{a^2}$$

No easy solutions for PSF under defocus.



## Strehl Limit

For **small** phase shifts, the PSF retains its  $|J(r)/r|^2$  shape but

- Zero do not move
- Peak value drops
- Subsidiary maximas rise

Define the **Strehl Limit** when central peak drops to **80%** of ideal. This occurs when phase difference

$$|\Delta\Phi(r)| \leq \frac{\pi}{4}$$

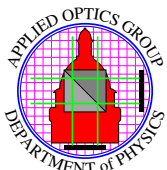
over the whole pupil function.

### Key Result

Systems that obey the Strehl limit are have “**good**” imaging properties, and is the standard design criteria for most good optical systems.

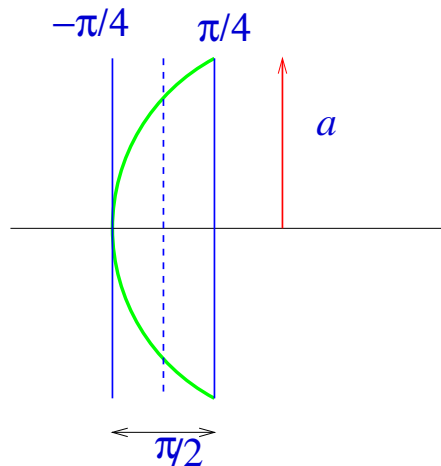
In terms of the Wavefront Aberration function,

$$\Delta\Phi(x,y) = \kappa W(x,y)$$



## Strehl Limit for Defocus

For defocus,



The Strehl Limit is that

$$\Delta\Phi_{\max} \leq \frac{\pi}{2}$$

Max phase error occurs at  $r = a$ , so

$$\Delta\Phi_{\max} = \kappa\Delta W = \frac{2\pi}{\lambda}\Delta W$$

So the Strehl limit for defocus is

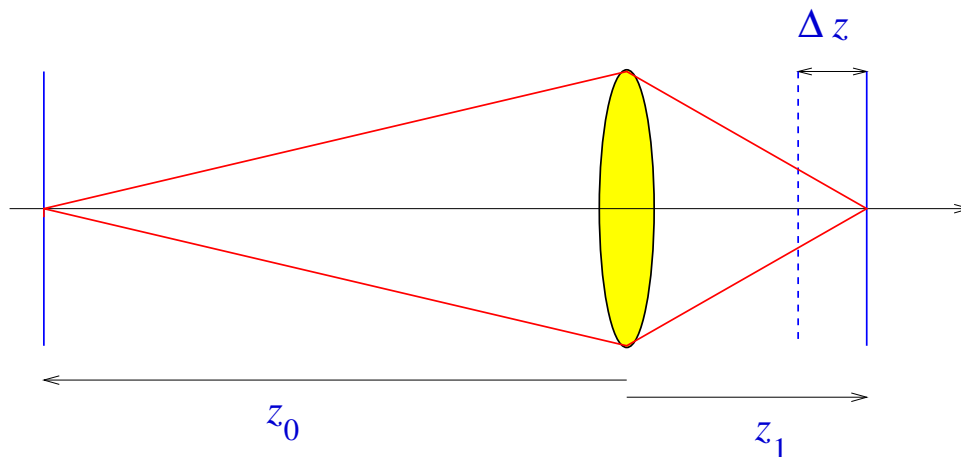
$$\Delta W < \frac{\lambda}{4}$$

This is equivalent to a max Optical Path Difference of  $\lambda/4$  over the aperture



## Object at a Finite Distance

Image is sharp focus with Image distance  $z_1$



Move image plane to  $z_1 - \Delta z$ , ( $\Delta z \ll z_1$ )

$$D = \frac{1}{z_0} - \frac{1}{f} + \frac{1}{z_1 - \Delta z} = \frac{1}{z_1 - \Delta z} - \frac{1}{z_1} \approx \frac{\Delta z}{z_1^2}$$

This gives that

$$\Delta W = \frac{1}{2} D a^2 = \frac{\Delta z}{2} \left( \frac{a}{z_1} \right)^2 < \frac{\lambda}{4}$$

so the **Strehl Limit** gives that

$$\Delta z \leq \frac{1}{2} \left( \frac{z_1}{a} \right)^2 \lambda$$

Special case when object at infinity,  $z_1 \rightarrow f$

$$\Delta z \leq \frac{1}{2} \left( \frac{f}{a} \right)^2 \lambda = 2F_{No}^2 \lambda$$

### Example:

Pocket camera, with  $f = 35\text{mm}$  and  $F_{No} = 3.5$ ,  $\Delta z = 13.5\mu\text{m}$  (about half the thickness of a human hair.)

## Other Aberrations

For On-axis points, system is cylindrically symmetric, so that

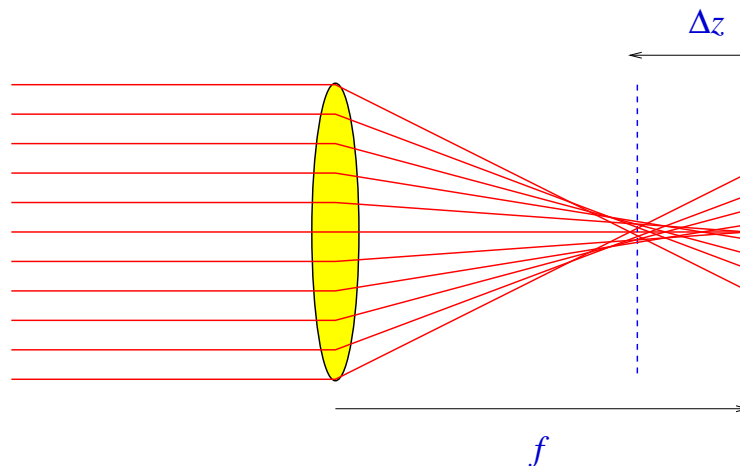
$$W(x, y) \quad \text{Even powers of } r$$

Taking terms to  $r^4$ , we get

$$W(x, y) = \frac{1}{8}S_1 \frac{(x^2 + y^2)^2}{a^4} + \Delta W \frac{(x^2 + y^2)}{a^2}$$

The  $S_1$  term is known as Spherical Aberration.

**Physical Explanation:** Lens surfaces are Spherical, NOT parabolic so outer rays focused “short”



Should be able to “improve” PSF by moving the image plane short of the ideal (paraxial) focus.

## Strehl Limit for Spherical Aberration

### 1) No Defocus:

$$W(r) = \frac{1}{8}S_1 \left(\frac{r}{a}\right)^4$$

Phase error then equals

$$\Delta\Phi(r) = \kappa W(r) = \frac{\pi}{4\lambda}S_1 \left(\frac{r}{a}\right)^4$$

As for defocus, Strehl limit is that

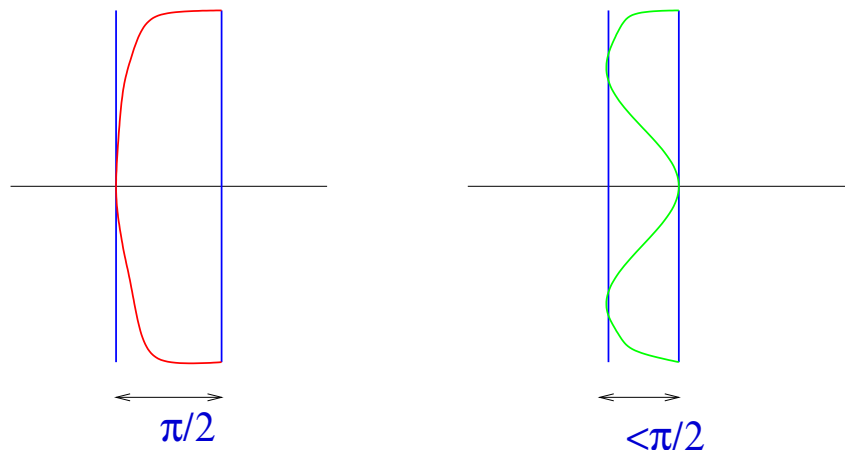
$$\Delta\Phi_{\max} \leq \frac{\pi}{2}$$

so that the limit for Spherical Aberration is

$$S_1 \leq 2\lambda$$

### 2) With Defocus:

Able to “cancel” some of the Spherical Aberration with defocus



cont: We can find optimal defocus by least squares minimisation of

$$\int_0^a |rW(r)|^2 dr$$

which “can-be-shown” to give the best PSF at

$$\Delta W = -\frac{7}{72}S_1$$

Minimum and maximum of phase function occurs at

$$r = \sqrt{\frac{7}{18}}a \quad \& \quad r = a$$

This gives a **Strehl Limit** of

$$S_1 \leq 5.36\lambda$$

Which is more than twice the limit if there is no defocus.

**Aside:** If viewed from a purely ray optics model, we get that

$$\Delta W = -\frac{1}{8}S_1$$

and the **Strehl Limit for Spherical Aberration** is

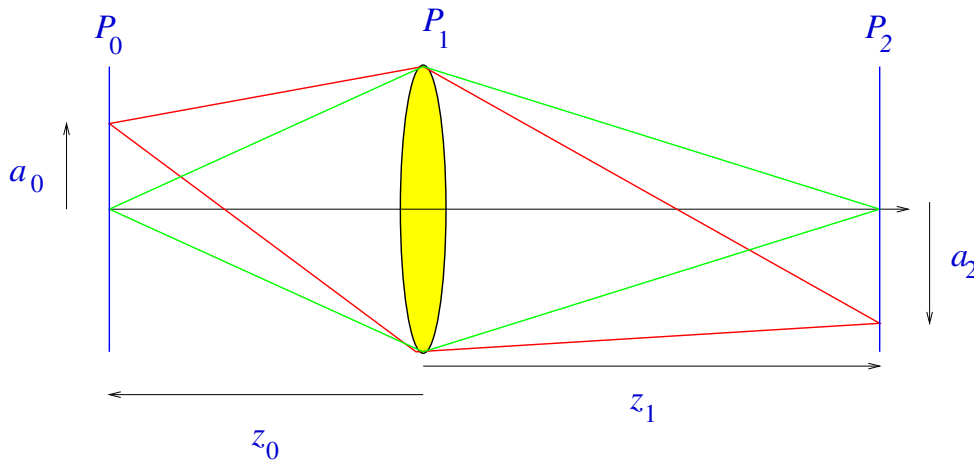
$$S_1 \leq 7.6\lambda$$

which is a similar result.

## Off Axis Points

### 1) Ideal Case:

PSF moves linearly and does not change shape



System is said to be **Space Invariant**, and

$$a_2 = -\frac{z_1}{z_0}a_0 = -Ma_0$$

Where  $M = z_1/z_2$  is the magnification of the system.

If the Object is a  $\delta$ -function at  $(a_0, b_0)$  then in plane  $P_2$  we get amplitude

$$u_2(x - a_2, y - b_2)$$

where  $u_2(x, y)$  is amplitude for  $\delta$ -function on axis and

$$a_2 = -\frac{z_1}{z_0}a_0 \quad \& \quad b_2 = -\frac{z_1}{z_0}b_0$$

## Practical Case

Shape of Pupil function will change,

- On-axis  $P(x,y)$  is circular.
- Off-axis  $P(x,y)$  is an ellipse.

So the PSF will change.

**Compound Lenses:** Effective shape of Pupil Function will change much more rapidly due to three dimensional nature of lens.

Result known as **Vignetting**. Major problem with very wide angle lenses which leads to edges of image being dull.

## Off-Axis Aberrations

No cylindrical symmetry, so much more complicated aberration problems.

Range of aberrations that depend on the object location, full form for First Order aberrations become,

$$W(x, y; \eta) = \frac{1}{2}S_0 \left( \frac{r^2}{a^2} \right) + \frac{1}{8}S_1 \left( \frac{r^4}{a^4} \right) + \frac{1}{2}S_2 \frac{yr^2}{a^3} \eta + \frac{1}{2}S_3 \frac{y^2}{a^2} \eta^2 + \frac{1}{4}(S_3 + S_4) \left( \frac{r^2}{a^2} \right) \eta^2 + \frac{1}{2}S_5 \frac{y}{a} \eta^3$$

where the terms are

1.  $\eta$  Off-Axis angle as fraction of maximum
2.  $S_0$  Defocus, same as  $2\Delta W$
3.  $S_1$  Spherical Aberration
4.  $S_2$  Coma
5.  $S_3$  Astigmatism
6.  $S_4$  Field Curvature
7.  $S_5$  Distortion.

Shape of PSF under these aberrations is difficult to calculate.